



THO4-P181 MIRI Cooler System Design Update

May 20, 2010

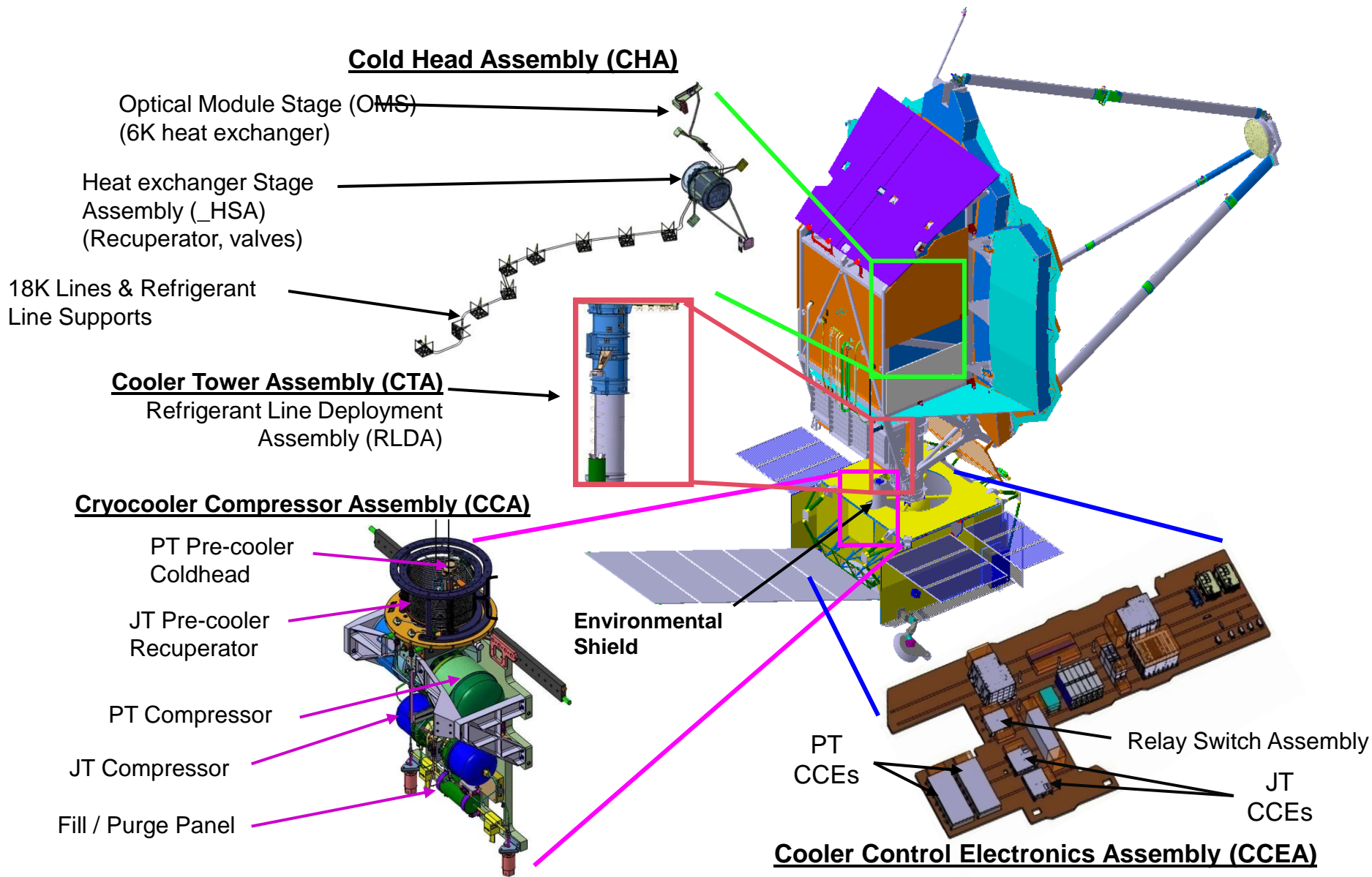
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Northrop Grumman Aerospace Systems**

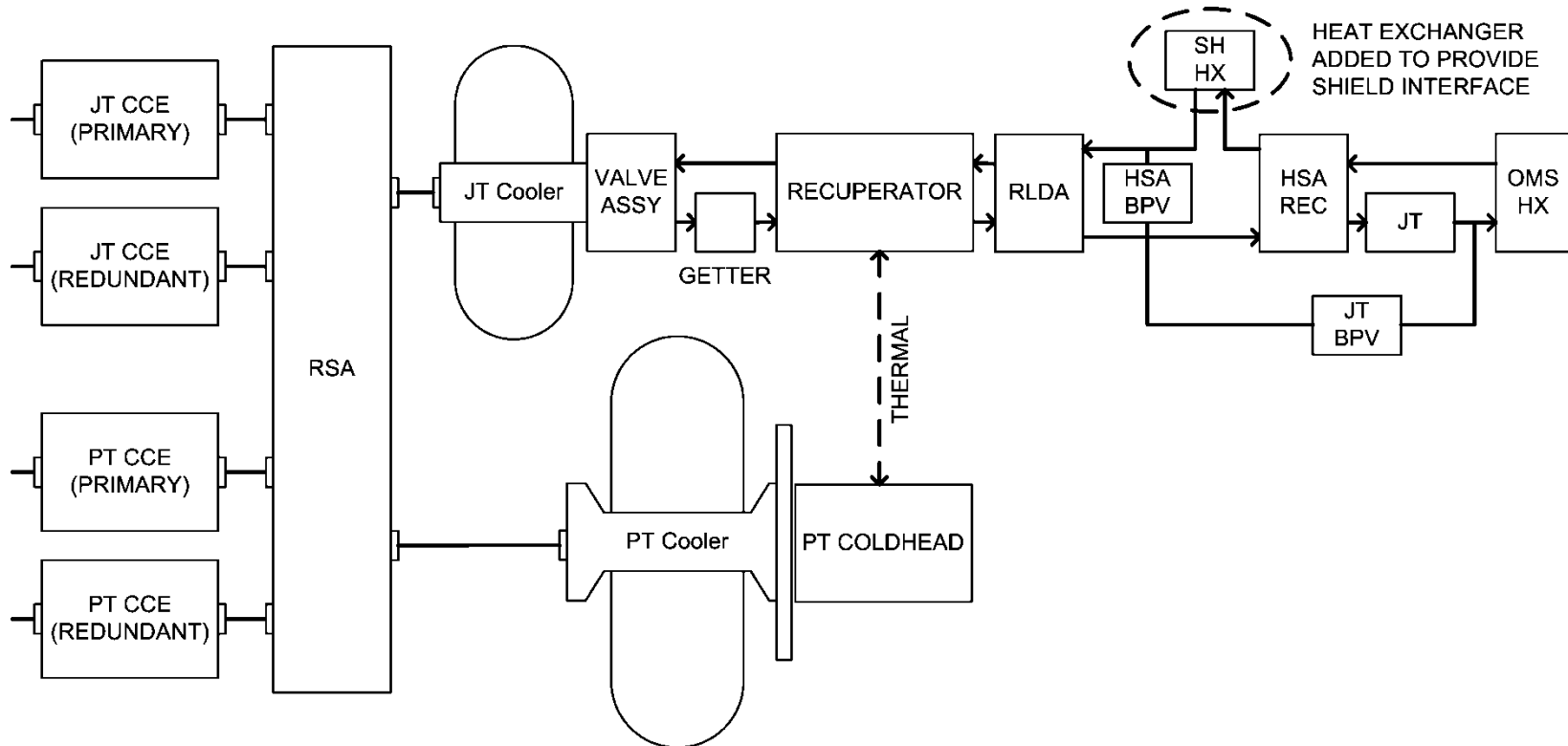
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MIRI Cooler Subsystem



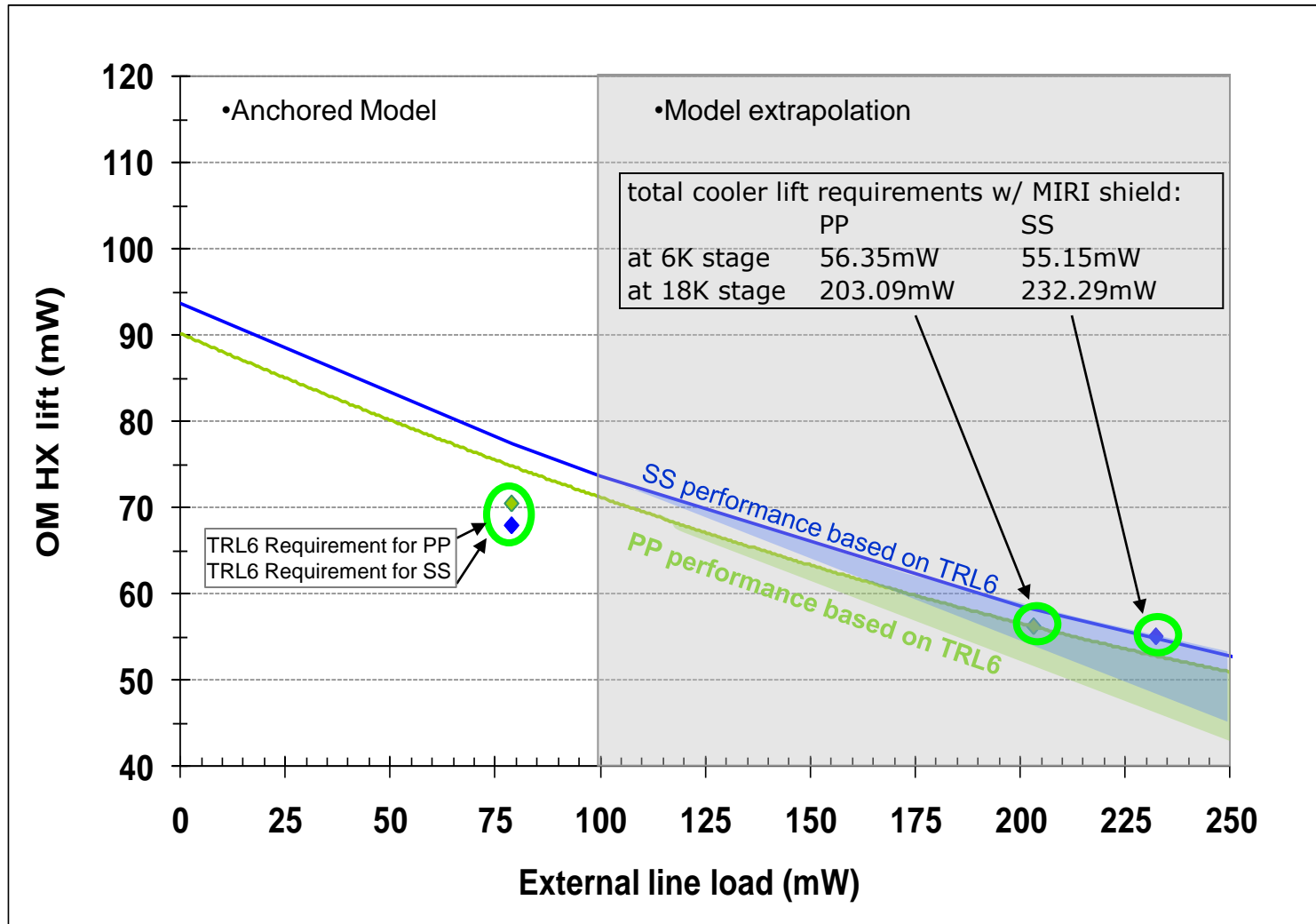


- **Heat Exchanger Added to Provide Interface to Actively Cooled Thermal Shield**
 - Shield surrounds the MIRI OM to intercept thermal radiation and reduce the OM thermal load
 - Heat added at shield heat exchanger is equivalent to extra parasitic load on the refrigerant lines (including the RLDA)
 - Change to design leads to a large increase in the effective line load, a reduction in the OM load at 6.2 K, for a net increase in cooler requirement



Anchored TRL 6 Model Extrapolated to New Requirements

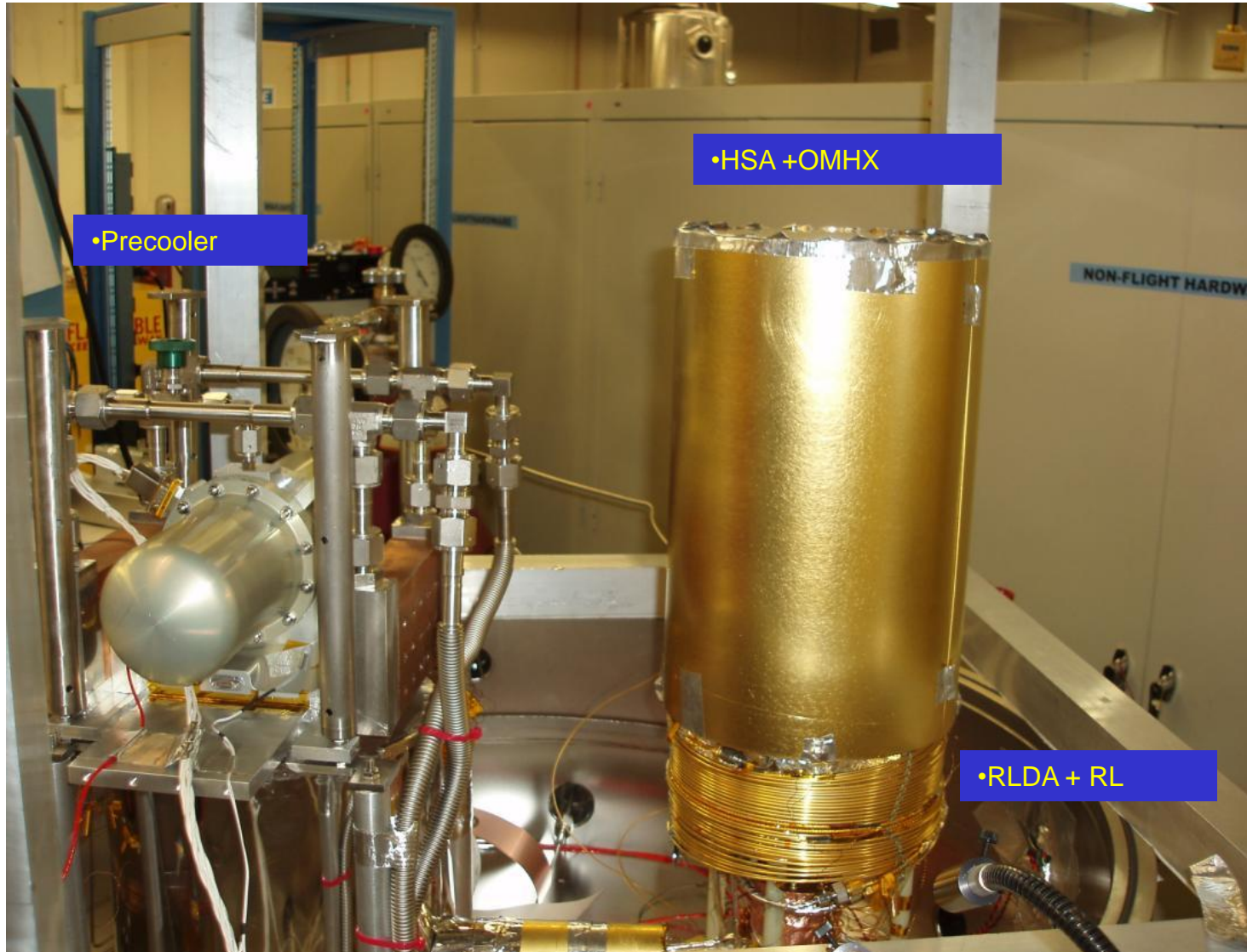
- Model anchored with TRL 6 test data used to extrapolate to region of new requirements
- New requirements are far outside the range previously characterized





DM cooler test photos

- DM test TMU with 40K ISIM Shield Removed





Prototype Joule-Thomson Compressor

- Flight-like construction and manufacturing processes
- Design changes led to efficiency improvement over previous laboratory version used in TRL 6 testing





Summary of Key DM Test Measurements



- The measured OM HX lift vs Line Load data is summarized in the table below
- The local slope of the OM HX lift vs Load allows extrapolation to other line loads
- The cooler has met the requirements of the test with
 - -0.3mW of OM HX lift for the “Strap” interface
 - +7.4mW of OM HX lift for the “HX” interface

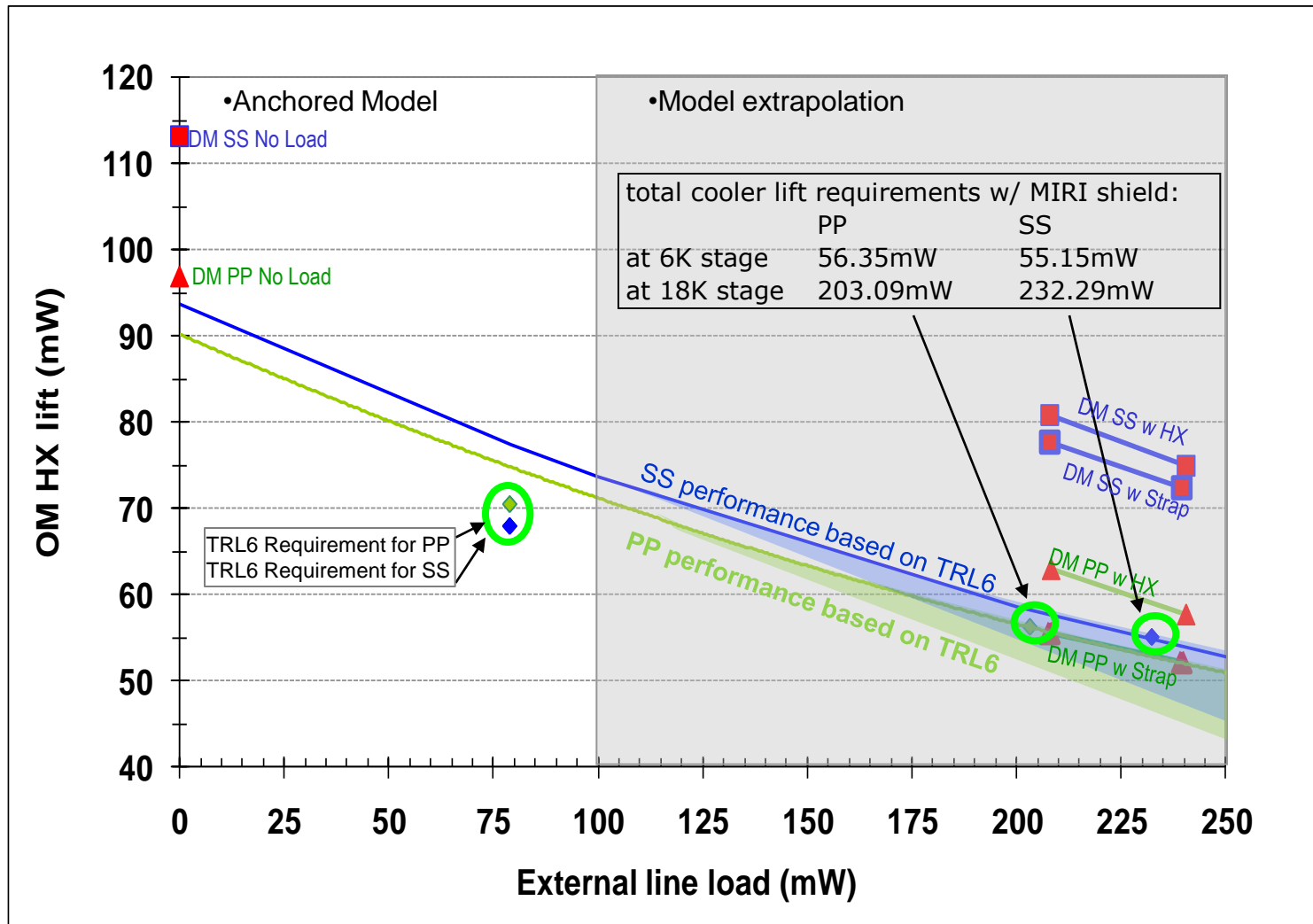
Measured							Extrapolated to current requirements			
Mode	Line Load	OM Lift	OM Temp	HSA T	Bus Power	Trej	Local slope	Line Load	OM Lift	OM req
Strap at Pinch Point							Strap at Pinch Point			
Strap PP	239mW	52mW	19.9K	20.0K	476 W	310K	-0.110mW/mW	203.1mW	56.1mW	56.4mW
Strap PP	208mW	56mW	19.0K	19.2K	471 W	310K				
No Load PP	0mW	97mW	15.2K	13.9K	470 W	310K				
Strap at Steady State							Strap in Steady State			
Strap SS	239mW	72mW	6.2K	22.0K	400 W	306K	-0.164mW/mW	232.3mW	73.6mW	55.2mW
Strap SS	208mW	78mW	6.2K	21.3K	400 W	306K				
No Load SS	0mW	113mW	6.2K	17.2K	395 W	307K				
HX at Pinch Point							HX at Pinch Point			
HX PP	241mW	58mW	19.1K	19.2K	475 W	310K	-0.160mW/mW	203.1mW	63.8mW	56.4mW
HX PP	208mW	63mW	18.3K	18.4K	476 W	310K				
No Load PP	0mW	97mW	15.2K	13.9K	470 W	310K				
HX at Steady State							HX at Steady State			
HX SS	241mW	75mW	6.2K	21.7K	400 W	306K	-0.159mW/mW	232.3mW	76.2mW	55.2mW
HX SS	208mW	81mW	6.2K	20.9K	400 W	306K				
No Load SS	0mW	113mW	6.2K	17.2K	395 W	307K				



DM Test Results Compared to Predictions



- Data in red shown on same graph as previous predictions indicate improvement due to heat exchanger approach and other design improvements





Summary of Performance Demonstration

- **Measurements Demonstrate MIRI Cooler Capability Meets New Requirements**
 - Steady State and Pinch Point requirements met for both options of thermal interface to OM shield
 - Heat exchanger approach shown to have improved performance over conductive strap approach—enables margin at the cooler level
- **Adaptation of Design Demonstrates Utility Over Range of Heat Loads**
 - Design capable of changing balance between intermediate temperature load and low temperature load without changing compressor or electronics designs
 - Model successfully used to guide design modification and accurately predicts performance—can be used to estimate performance in other space astronomy applications